# **Smoothing of sandpile surfaces after intermittent and continuous avalanches: Three models in search of an experiment**

Parthapratim Biswas\* and Arnab Majumdar†

*S. N. Bose National Centre For Basic Sciences, Salt Lake City, Block JD, Sector III, Calcutta 700 091, India*

Anita Mehta‡

*S. N. Bose National Centre For Basic Sciences, Salt Lake City, Block JD, Sector III, Calcutta 700 091, India and Institute of Theoretical Physics, University of California, Santa Barbara, California 93106*

# J. K. Bhattacharjee§

*Department of Theoretical Physics, Indian Association for the Cultivation of Science, Jadavpur, Calcutta 700 032, India* (Received 21 August 1997)

We present and analyze in this paper three models of coupled continuum equations all united by a common theme: the intuitive notion that sandpile surfaces are left smoother by the propagation of avalanches across them. Two of these concern smoothing at the ''bare'' interface, appropriate to intermittent avalanche flow, while one of them models smoothing at the effective surface defined by a cloud of flowing grains across the ''bare'' interface, which is appropriate to the regime where avalanches flow continuously across the sandpile.  $[S1063-651X(98)07205-5]$ 

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### **I. INTRODUCTION**

The dynamics of sandpiles have intrigued researchers in physics over recent years  $[1,2]$  with a great deal of effort being devoted to the development of techniques involving, for instance, cellular automata  $[3,4]$ , continuum equations  $[5-7]$ , and Monte Carlo schemes  $[8]$  to investigate this very complex subject. However, what have often been lost sight of in all this complexity are some of the extremely simple phenomena that are exhibited by granular media, which still remain unexplained.

One such phenomenon is that of the smoothing of a sandpile surface after the propagation of an avalanche  $[9]$ . It is clear what happens physically: an avalanche provides a means of shaving off roughness from the surface of a sandpile by transferring grains from bumps to available voids [2,4], and thus leaves in its wake a smoother surface. However, surprisingly, researchers have not to our knowledge come up with models of sandpiles that have exhibited this behavior.

In particular what has not attracted enough attention in the literature is the qualitative difference between the situations that are obtained when sandpiles exhibit intermittent and continuous avalanches  $[10]$ . In this paper we examine both of the latter situations, via distinct models of sandpile surfaces.

A particular experimental paradigm that we choose to put

§ Electronic address: tpjkb@iacs.ernet.in

 $[11,12]$ . In the case when sand is rotated slowly in a cylinder, intermittent avalanching is observed; thus sand accumulates in part of the cylinder to beyond its angle of repose  $\lceil 13 \rceil$  and is then released via an avalanche process across the slope. This happens intermittently, since the rotation speed is less than the characteristic time between avalanches. By contrast, when the rotation speed exceeds the time between avalanches, we see continuous avalanching on the sandpile surface. Though this phenomenon has been observed  $[13]$  and analyzed physically  $[10]$  in terms of avalanche statistics, we are not aware of measurements which measure the characteristics of the resulting surface in terms of its smoothness or otherwise.

our discussions in context is that of sand in rotating cylinders

What we focus on here is precisely this aspect, and make predictions that we hope will be tested experimentally. In order to discuss this, we introduce first the notion that granular dynamics is well described by the competition between the dynamics of grains moving independently of each other and that of their collective motion within clusters  $[2]$ . A convenient way of representing this is via coupled continuum equations with a specific coupling between mobile grains  $\rho$ and clusters  $h$  on the surface of a sandpile  $[5]$ . In the regime of intermittent avalanching, we expect that the interface will be the one defined by the ''bare'' surface, i.e., the one defined by the relatively immobile clusters across which grains flow intermittently. This then implies that the roughening characteristics of the *h* profile should be examined. The simplest of the three models we discuss in this paper (an exactly solvable model referred to hereafter as case *A*) as well as the most complex one (referred to hereafter as case  $C$ ) treat this situation, where we obtain in both cases an asymptotic smoothing behavior in *h*. When, on the other hand, there is continuous avalanching, the flowing grains provide an effective film across the bare surface and it is therefore the species  $\rho$  that should be analyzed for spatial and temporal roughening. In the model hereafter referred to as case *B* we look at this situation, and obtain the surprising result of a gradual

<sup>\*</sup>Electronic address: ppb@boson.bose.res.in

<sup>†</sup> Present address: Physics Department, Boston University, Boston, MA 02215. Electronic address: arnab@bu.edu

<sup>‡</sup> Author to whom correspondence should be addressed. Present address: Clarendon Laboratory, Parks Rd., Oxford OX1 3PU, U.K. Electronic address: a.mehta1@physics.ox.ac.uk

In general, the complexity of sandpile dynamics leads us to equations that are coupled, nonlinear, and noisy: these equations present challenges to the theoretical physicist in more ways than the obvious ones that pertain to their detailed analysis and/or their numerical solutions. In particular, our analysis of case *C* reveals the presence of hidden length scales whose existence was suspected analytically, but not demonstrated numerically in earlier work  $[5,14]$ .

The normal procedure for probing temporal and spatial roughening in interface problems is to determine the asymptotic behavior of the interfacial width with respect to time and space, via the single Fourier transform. Here only one of the variables, (*x*,*t*), is integrated over in Fourier space, and appropriate scaling relations are invoked to determine the critical exponents that govern this behavior. However, it turns out that this leads to ambiguities for those classes of problems where there is an absence of simple scaling, or to be more specific, where multiple length scales exist. In such cases we demonstrate that the double Fourier transform (where *both* time and space are integrated over) yields insights that are harder to obtain via the single Fourier transform.

This point is illustrated by case *A*, an exactly solvable model that we introduce; we then use it to understand case *C*, a nonlinear model where our analytical results are clearly only approximations to the truth.

In order to make some of these ideas more concrete, we now review some general facts about rough interfaces [15]. Three critical exponents,  $\alpha$ ,  $\beta$ , and *z*, characterize the spatial and temporal scaling behavior of a rough interface. They are conveniently defined by considering the (connected) twopoint correlation function of the heights

$$
S(x-x',t-t') = \langle h(x,t)h(x',t')\rangle - \langle h(x,t)\rangle \langle h(x',t')\rangle.
$$
\n(1)

We have

$$
S(x,0) \sim |x|^{2\alpha}
$$
  $(|x| \to \infty)$  and  $S(0,t) \sim |t|^{2\beta}$   $(|t| \to \infty)$ ,

and more generally

$$
S(x,t) \approx |x|^{2\alpha} F(|t|/|x|^z)
$$

in the whole long-distance scaling regime  $(x \text{ and } t \text{ large})$ . The scaling function  $F$  is universal in the usual sense;  $\alpha$  and  $z = \alpha/\beta$  are respectively referred to as the roughness exponent and the dynamical exponent of the problem. In addition, we have for the full structure factor, which is the double Fourier transform  $S(k,\omega)$ ,

$$
S(k,\omega)\sim \omega^{-1}k^{-1-2\alpha}\Phi(\omega/k^{z}),
$$

which gives in the limit of small  $k$  and  $\omega$ ,

$$
S(k, \omega = 0) \sim k^{-1 - 2\alpha - z}(k \to 0) \quad \text{and}
$$
  

$$
S(k = 0, \omega) \sim \omega^{-1 - 2\beta - 1/z} \quad (\omega \to 0).
$$
 (2)

The scaling relations for the corresponding single Fourier transforms are

$$
S(k,t=0) \sim k^{-1-2\alpha}(k \to 0) \quad \text{and}
$$
  

$$
S(x=0,\omega) \sim \omega^{-1-2\beta} \quad (\omega \to 0).
$$
 (3)

In particular we note that the scaling relations for  $S(k,\omega)$ [Eq. (2)] always involve the simultaneous presence of  $\alpha$  and  $\beta$ , whereas those corresponding to  $S(x, \omega)$  and  $S(k, t)$  involve these exponents *individually*. Thus, in order to evaluate the double Fourier transforms, we need in each case information from the growing as well as the saturated interface (the former being necessary for  $\beta$  and the latter for  $\alpha$ ) whereas for the single Fourier transforms, we need only information from the saturated interface for  $S(k,t=0)$  and information from the growing interface for  $S(x=0,\omega)$ . On the other hand, the information that we will get out of the double Fourier transform will provide a more unambiguous picture in the case where multiple length scales are present, something that cannot easily be obtained in every case with the single Fourier transform.

In Secs. II, III, and IV we present, analyze, and discuss the results of cases *A*, *B*, and *C*, respectively. Finally, in Sec. V, we reflect on the unifying features of these models, and make some educated guesses on the dynamical behavior of real sandpile surfaces.

# **II. CASE** *A***: THE EDWARDS-WILKINSON EQUATION WITH FLOW**

Our first model involves a pair of linear coupled equations, where the equation governing the evolution of clusters ~''stuck'' grains! *h* is closely related to the very well-known Edwards-Wilkinson  $(EW)$  model [16]. The equations are

$$
\frac{\partial h(x,t)}{\partial t} = D_h \nabla^2 h(x,t) + c \nabla h(x,t) + \eta(x,t), \qquad (4a)
$$

$$
\frac{\partial \rho(x,t)}{\partial t} = D_{\rho} \nabla^2 \rho(x,t) - c \nabla h(x,t),\tag{4b}
$$

where the first of the equations describes the height  $h(x,t)$  of the sandpile surface at  $(x,t)$  measured from some mean  $\langle h \rangle$ , and is precisely the EW equation in the presence of the flow term  $c\nabla h$ . The second equation describes the evolution of flowing grains, where  $\rho(x,t)$  is the local density of such grains at any point  $(x,t)$ . As usual, the noise  $\eta(x,t)$  is taken to be Gaussian so that

$$
\langle \eta(x,t) \eta(x',t') \rangle = \Delta^2 \delta(x-x') \delta(t-t'),
$$

with  $\Delta$  the strength of the noise. Here,  $\langle \cdots \rangle$  refers to an average over space as well as over noise.

#### **A. Analysis of the decoupled equation in** *h*

For the purposes of analysis, we focus on the first of the two coupled equations  $[Eq. (4a)]$  presented above,

$$
\frac{\partial h}{\partial t} = D_h \nabla^2 h + c \nabla h + \eta(x, t)
$$



FIG. 1. The correlation function  $S_h(k_i, \omega)$  against  $\omega$  for three different wave vectors  $k_1 = 0.02$  ( $\diamond$ ),  $k_2 = 0.08$  (+), and  $k_3$ = 0.12 ( $\square$ ) with parameters *c* = 2.0,  $D_h$  = 1.0, and  $\Delta^2$  = 1.0. The positions of the peaks are given by  $\omega_1$  = 0.04,  $\omega_2$  = 0.16, and  $\omega_3$ =0.24 as expected from Eq. (5).

noting that this equation is essentially decoupled from the second. (This statement is, however, not true in reverse, which has implications to be discussed later.) We note that this is entirely equivalent to the Edwards-Wilkinson equation [16] in a frame moving with velocity  $c$ ,

$$
x' = x + ct, \quad t' = t,
$$

and we would on these grounds expect to find only the wellknown EW exponents  $\alpha$ =0.5 and  $\beta$ =0.25 [16]. This would be verified by naive single Fourier transform analysis of Eq.  $(4a)$  which yields these exponents via Eq.  $(3)$ .

Equation  $(4a)$  can be solved exactly as follows. The propagator  $G(k,\omega)$  is

$$
G_h(k,\omega) = (-i\omega + D_h k^2 + ikc)^{-1}.
$$

This can be used to evaluate the structure factor

$$
S_h(k,\omega) = \frac{\langle h(k,\omega)h(k',\omega')\rangle}{\delta(k+k')\,\delta(\omega+\omega')},
$$

which is the Fourier transform of the full correlation function  $S_h(x-x', t-t')$  defined by Eq. (1). The solution for  $S_h(k,\omega)$  so obtained is

$$
S_h(k,\omega) = \frac{\Delta^2}{(\omega - ck)^2 + D_h^2 k^4}.
$$
 (5)

This is illustrated in Fig. 1 while representative graphs for  $S_h(k, \omega=0)$  and  $S_h(k=0, \omega)$  are presented in Figs. 2 and 3, respectively. Before proceeding further, we make the following observation about the double Fourier transform  $S_h(k=0,\omega)$ ; this shows an  $\omega^{-2}$  behavior coming from Eq.  $(5)$ , which we will also see later. We mention here that the ubiquity of this  $\omega^{-2}$  arises from the form of the scaling relation Eq. (2), which is relevant for frequencies  $\omega < \omega_c$  $\approx k^{z_h}$ , whereas for  $\omega > \omega_c$  the high frequency behavior takes over giving  $\omega^{-2}$  [cf. Eq. (A2) in the Appendix]. As  $k=0$  for the purposes of calculation of this structure factor, it is always the high frequency behavior that dominates, leading to the ubiquity of  $\omega^{-2}$  whenever it is measured.

It is obvious from Eq. (5) that  $S_h(k,\omega)$  does not show simple scaling. More explicitly, if we write

$$
S_h^{-1}(k, \omega = 0) = \frac{\omega_0^2}{\Delta^2} \left(\frac{k}{k_0}\right)^2 \left[1 + \left(\frac{k}{k_0}\right)^2\right]
$$

with  $k_0 = c/D_h$ , and  $\omega_0 = c^2/D_h$ , we see that there are two limiting cases :

- (i) for  $k \ge k_0$ ,  $S_h^{-1}(k, \omega = 0) \sim k^4$ ; using again  $S_h^{-1}(k)$  $(50, \omega) \sim \omega^2$ , we obtain  $\alpha_h = 1/2$  and  $\beta_h = 1/4$ ,  $z_h = 2$ via Eqs.  $(2)$ .
- (ii) for  $k \ll k_0$ ,  $S_h^{-1}(k, \omega = 0) \sim k^2$ ; using the fact that the limit  $S_h^{-1}(k=0,\omega)$  is always  $\omega^2$ , this is consistent with the set of exponents  $\alpha_h=0$ ,  $\beta_h=0$ , and  $z_h=1$ via Eqs.  $(2)$ .

The first of these contains no surprises, being the normal EW fixed point  $[16]$ , while the second represents a new, ''smoothing'' fixed point.

We now explain this smoothing fixed point via a simple physical picture. The competition between the two terms in Eq.  $(4a)$  determines the nature of the fixed point observed: when the diffusive term dominates the flow term, the canonical EW fixed point is obtained, in the limit of large wave vectors *k*. On the contrary, when the flow term predominates, the effect of diffusion is suppressed by that of a traveling wave whose net result is to penalize large slopes; this leads to the smoothing fixed point obtained in the case of small wave vectors *k*. We emphasize, however, that this is a toy model of smoothing, which will be used to illuminate the discussion of models *B* and *C* below.



FIG. 2. The double Fourier transform,  $S_h(k, \omega=0)$  obtained from Eq. (4) (Case A), plotted on a log-log scale to show the crossover from  $k^{-2}$  at low wave vectors to  $k^{-4}$  at high wave vectors. The different markers in the figure correspond to different grid sizes  $\Delta x$  to sample distinct regions of *k* space; thus the markers  $\triangle$  and  $\square$  correspond to decreasing grid sizes and increasing wave-vector ranges. The parameters used in the calculation are  $c = D_h = \Delta^2 = 1.0$  and the characteristic wave vector is  $k_0 = c/D_h = 1.0$ . The dashed line is a plot of the theoretical  $S_h(k, \omega=0)$  for Case A with appropriate parameters, to serve as a guide to the eye.

### **B. Coupled equations: A model of smoothing**

We realize from the above that the interface *h* is smoothed because of the action of the flow term, which penalizes the sustenance of finite gradients  $\nabla h$  in Eq. (4a). However, Eq.  $(4a)$  is effectively decoupled from Eq.  $(4b)$ , while Eq.  $(4b)$  is manifestly coupled to Eq.  $(4a)$ . In order for the coupled Eqs.  $(4)$  to qualify as a valid model of sandpile dynamics, we would need to ensure that no instabilities are generated in either of these by the coupling term  $c \nabla h$ .

In this spirit, we look first at the value of  $\rho$  averaged over the sandpile, as a function of time [Fig. 4(a)]. We observe that the incursions of  $\langle \rho \rangle$  into negative values are limited to relatively small values, suggesting that the addition of a constant background of  $\rho$  exceeding this negative value would render the coupled system meaningful, at least to a first approximation. In order to ensure that this average does not involve wild fluctuations, we examine the fluctuations in  $\rho$ , viz.,  $\sqrt{\langle \rho^2 \rangle - \langle \rho \rangle^2}$  [Fig. 4(b)]. The trends in that figure indicate that this quantity appears to saturate, at least up to computationally accessible times. Finally we look at the *minimum* and *maximum* value of  $\rho$  at any point in the pile over a large range of times [Fig.  $4(c)$ ]; this appears to be bounded



FIG. 3. The double Fourier transform  $S_h(k=0,\omega)$  vs  $\omega$  obtained from Eq. (4) (Case A) plotted on a log-log scale. The different markers in the figure correspond to different grid sizes  $\Delta t$  to sample distinct regions of  $\omega$  space, as in Fig. 2. The solid line is a plot of the theoretical  $S_h(k=0,\omega) \sim \omega^{-2}$  for case A with appropriate parameters, to serve as a guide to the eye. The parameters are  $c = D_h = \Delta^2 = 1.0$ .



FIG. 4. (a) The behavior of  $\langle \rho(t) \rangle$  as a function of time *t*. Here  $\langle \rho(t) \rangle$  is the average over the sandpile surface of 100 sample configurations. The grid size  $\Delta t = 0.005$  and  $c = \Delta^2 = D_h = 1.0$ . (b) The root mean square width  $\rho_{\rm rms}(t) = (\langle \rho^2 \rangle - \langle \rho \rangle^2)^{1/2}$  against time *t* over 100 sample configurations with parameters  $c = \Delta^2 = D_\rho = D_h = 1.0$ . (c) The variation of  $\rho_{\text{max}}(t)$  and  $\rho_{\text{min}}(t)$  with time *t*.  $\rho_{\text{max}}(t)$  and  $\rho_{\text{min}}(t)$  are respectively the maximum and minimum values of  $\rho$  for a given configuration of the sandpile at time *t*. Again,  $c = D_h = D_\rho = \Delta^2 = 1.0$ .

by a modest (negative) value of "bare"  $\rho$ . Our conclusions are thus that the fluctuations in  $\rho$  saturate at computationally accessible times and that the negativity of the fluctuations in  $\rho$  can always be handled by starting with a constant  $\rho_0$ , a constant ''background'' of flowing grains, which is more positive than the largest negative fluctuation.

Physically, then, the above implies that at least in the presence of a constant large density  $\rho_0$  of flowing grains, it is possible to induce the level of smoothing corresponding to the fixed point  $\alpha = \beta = 0$ . This model is thus one of the simplest possible ways in which one can obtain a representation of the smoothing of the ''bare surface'' that is frequently observed in experiments on real sandpiles after intermittent avalanche propagation  $[9]$ .

# **III. CASE** *B***: A SIMPLE FORM OF COUPLING, WITH COMPLEX CONSEQUENCES**

Our model equations, first presented in  $[5]$ , involve a simple coupling between the species  $h$  and  $\rho$ , where the transfer between the species occurs only in the presence of the flowing grains and is therefore relevant to the regime of continuous avalanching when the duration of the avalanches is *large* compared to the time between them. The equations are

$$
\frac{\partial h(x,t)}{\partial t} = D_h \nabla^2 h(x,t) - T(h,\rho) + \eta_h(x,t), \qquad (6a)
$$

$$
\frac{\partial \rho(x,t)}{\partial t} = D_{\rho} \nabla^2 \rho(x,t) + T(h,\rho) + \eta_{\rho}(x,t), \qquad (6b)
$$

$$
T(h,\rho) = -\mu \rho(\nabla h),\tag{6c}
$$

where the terms  $\eta_h(x,t)$  and  $\eta_\rho(x,t)$  represent Gaussian white noise as usual:

$$
\langle \eta_h(x,t) \eta_h(x',t') \rangle = \Delta_h^2 \delta(x-x') \delta(t-t'),
$$
  

$$
\langle \eta_\rho(x,t) \eta_\rho(x',t') \rangle = \Delta_\rho^2 \delta(x-x') \delta(t-t'),
$$

and  $\langle \cdots \rangle$  stands for average over space as well as noise.

A simple physical picture of the coupling or ''transfer'' term  $T(h,\rho)$  between *h* and  $\rho$  is the following: flowing grains are added in proportion to their local density to regions of the interface that are at less than the critical slope, and vice versa, *provided that the local density of flowing grains is always nonzero*. This form of interaction becomes zero in the absence of a finite density of flowing grains  $\rho$ (when the equations become decoupled) and is thus the simplest form appropriate to the situation of continuous avalanching in sandpiles. We analyze in the following the profiles of  $h$  and  $\rho$  consequent on this form.

It turns out that a singularity discovered by Edwards  $[18]$ three decades ago in the context of fluid turbulence is present in models with a particular form of the transfer term *T*; the above is one example, while another example is the model due to Bouchaud *et al.* (BCRE) [7], where

$$
T = -\nu \nabla h - \mu \rho (\nabla h)
$$

and the noise is present only in the equation of motion for *h*. This singularity, the so-called infrared divergence, largely controls the dynamics and produces unexpected exponents.

### **A. Theoretical analysis**

We carry out first the theoretical analysis of Eqs.  $(6)$ . An examination of the above equations reveals the presence of two likely length scales in each, one associated with the diffusive motion, and the other with the so-called transfer term  $T(h,\rho)$ , representing the coupling between the two species. In these circumstances, a renormalization group analysis would clearly be inappropriate due to the breakdown of simple scaling. In recent years, however, a self-consistent mode coupling analysis used hitherto in dynamic critical phenomena  $[19]$  has been used to look at, in particular, the Kardar-Parisi-Zhang  $(KPZ)$  equation  $[17,20]$  and we extend its use to the case of the coupled equations presented here.

In this method we set up equations (to one-loop order) for the correlation functions, and self-energies in terms of the full Green's functions, correlation functions, and vertices using assumed scaling forms for each. The critical exponents  $\alpha$ and  $\beta$  defined above are obtained from the self-consistent solutions of these equations using  $D_h = D_\rho$ .

Focusing on the *h* variable to start with, we define the Green's functions and the correlation functions of the *h* and  $\rho$  variables

$$
G_h(k,\omega) = \left\langle \frac{\partial h(k,\omega)}{\partial \eta(k',\Omega)} \right\rangle \frac{1}{\delta(k+k')\delta(\omega+\Omega)},
$$
  

$$
G_\rho(k,\omega) = \left\langle \frac{\partial \rho(k,\omega)}{\partial \eta(k',\Omega)} \right\rangle \frac{1}{\delta(k+k')\delta(\omega+\Omega)},
$$
  

$$
S_h(k,\omega) = \frac{\langle h(k,\omega)h(k',\Omega) \rangle}{\delta(k+k')\delta(\omega+\Omega)},
$$
  

$$
S_\rho(k,\omega) = \frac{\langle \rho(k,\omega)\rho(k',\Omega) \rangle}{\delta(k+k')\delta(\omega+\Omega)}.
$$

The analysis of these functions will be in terms of a weak scaling hypothesis, which states

$$
G_h(k,\omega) = k^{-z_h} f_h\left(\frac{\omega}{k^{z_h}}, \frac{\omega}{k^{z_\rho}}\right),
$$
  

$$
G_\rho(k,\omega) = k^{-z_\rho} f_\rho\left(\frac{\omega}{k^{z_h}}, \frac{\omega}{k^{z_\rho}}\right).
$$

A strong scaling would imply the existence of a single time scale, i.e.,  $z_h = z_o$ . As we show below, this cannot be the case here. The absence of strong scaling implies that the roughness exponents  $\alpha_h$  and  $\alpha_o$  may become functions of *k*.

We consider the full Green's function  $G_h(k,\omega)$ , which is given via the well-known Dyson equation  $[21]$ ,

$$
G_h^{-1}(k,\omega) = G_h^{0-1}(k,\omega) + \sum_h(k,\omega).
$$

Here, the zeroth order Green's function is

$$
G_h^0(k,\omega) = (-i\omega + k^2)^{-1}.
$$

The scaling forms of the functions  $G_h(k,\omega)$  and  $S_h(k,\omega)$  are given by, in the limit  $\omega \rightarrow 0$ ,

$$
G_h(k,\omega)\sim \frac{1}{i\,\omega+k^2+k^{z_h}},
$$

$$
S_h(k,\omega)\sim\frac{1}{k^{1+2\alpha_h-z_h}}\left(\frac{1}{\omega^2+k^{2z_h}}\right).
$$

Similar scaling relations hold for the species  $\rho$ .

To one-loop order, the self-energy  $\Sigma_h(k)$  is given by [Fig.  $5(b)$ 

$$
\Sigma_h(k,\omega) = \mu^2 \int \frac{dq}{2\pi} \int \frac{d\Omega}{2\pi} G_h(k-q,\omega-\Omega) S_\rho(q,\Omega) k(k-q)
$$
\n(7a)

$$
\sim \mu^2 \int \frac{dq}{2\pi} \int \frac{d\Omega}{2\pi} \left[ \frac{1}{i(\omega - \Omega) + \Sigma_h (k - q, \omega - \Omega)} \right] \frac{k(k - q)}{q^{1 + 2\alpha_p}} \left[ \frac{2\Sigma_p(q, \Omega)}{\Omega^2 + |\Sigma_p(q, \Omega)|^2} \right],\tag{7b}
$$

where the second line follows from the first in the limit of small  $\Omega$ . We note that due to the presence of the term  $q^{-1-2\alpha_{\rho}}$ , the integral is dominated by the singularity in the integrand at  $q \rightarrow 0$ . This "infrared divergence," which results from the divergence of the *internal* momenta *q*, is very different from the usual divergences encountered in critical phenomena where the latter occur for small wave numbers and are associated with long wavelength instabilities in the external momenta. In this case due to the infrared divergence in the above equation in the internal momenta *q*, the integral diverges *for any value of the external momenta k*, so long as  $\alpha_{\rho}$ >0.

We thus need either to evaluate the integral with a lower cutoff  $k_0$  or to introduce a suitable regulator. We follow the first of these procedures for the above equation, and the second of the procedures to do with the corresponding quantity,  $S_{\rho}(k,\omega)$ , for  $\rho$ .

We then proceed to evaluate the self-energy at zero external frequency, i.e.,  $\sum_{h}(k,\omega=0)$  from Eq. (7a). As  $q\rightarrow 0$  we can approximate  $G_h(k-q,-\Omega)$  by

$$
G_h^{-1}(k, -\Omega) = i\Omega + k^2 + \Sigma_h(k, -\Omega)
$$

$$
\approx k^2 + \Sigma_h(k, 0),
$$

where the second line follows from the fact that we are looking at the  $q \approx 0$  limit of the internal frequency  $\Omega \sim q^{z_h}$ . As  $\sum_{h}$ (*k*,0) ~  $k^{z_h}$ , the small *k* behavior of  $G_h(k)$  is dominated by  $\Sigma_h(k)$  for  $z_h$ <2, i.e.,

$$
G_h^{-1}(k) \sim \Sigma_h(k).
$$

The integral in Eq.  $(7a)$  becomes in the limit of zero external frequencies

$$
\Sigma_h(k) = \frac{\mu^2 k^2}{\Sigma_h(k)} \int \frac{dq}{2\pi} \int \frac{d\Omega}{2\pi} S_\rho(q,\Omega).
$$

Using the scaling form for the single Fourier transform  $Eq.$  $(3)$ ] we find

$$
\Sigma_h(k) = \mu^2 k^2 \Sigma_h(k)^{-1} C_\rho \int \frac{dq}{2\pi} \frac{1}{q^{1+2\alpha_\rho}}.
$$

We now have to evaluate the integral by cutting off the momentum integration at  $k_0 \ll 1$ , i.e., we follow the first of the procedures given above to handle the infrared divergence. This gives, after some simplification,

$$
\Sigma_h^2(k) = \mu^2 k^2 \frac{k_0^{-2\alpha_\rho} C_\rho}{4\pi\alpha_\rho}.
$$

From the above equation with the scaling relation  $\Sigma_h(k)$  $\sim$ *k*<sup>*zh*</sup> we find, on equating powers of *k*,

$$
z_h = 1.
$$

We note here that the presence of the term  $\rho \nabla h$  could in principle cause the vertex  $\mu$  to renormalize, leading to a correction to  $z_h$ . In these circumstances, the expression for the self-energy  $\Sigma_h(k,\omega=0)$  is given by

$$
\Sigma_h(k,\omega=0) = \mu^2 \int \frac{dq}{2\pi} \int \frac{d\Omega}{2\pi} \Gamma_3(k,q,k-q)
$$

$$
\times G_h(k-q,-\Omega) S_\rho(q,\Omega) k(k-q), \qquad (8)
$$

where we have introduced a three-point vertex function  $\Gamma_3(k,q,k-q)$  in Eq. (7a). Assuming that as  $q\rightarrow 0$ , we can write the asymptotic form for the three-point vertex as

$$
\Gamma_3(k,q,k-q) \sim k^{x_\mu} \tag{9}
$$

we find

$$
z_h = 1 + \frac{x_\mu}{2}.
$$

In the event that numerical results suggest  $z_h \neq 1$  we will have to incorporate this new renormalized vertex into our calculations.

Next we examine the correlation function for  $h$ ,  $S_h(k,\omega)$ , which to one-loop order is given by  $[Fig. 6(a)]$ 



FIG. 5. One-loop diagrams for (a)  $\Sigma_{\rho}(k,\omega)$ , the self-energy in  $\rho$ , (b)  $\Sigma_h(k,\omega)$ , the self-energy in *h* for the coupled equations of case  $B$  [Eq.  $(6)$ ].  $(c)$  The glossary for the diagrams shown in  $(a)$  and (b) and Fig. 6. For example, the propagators for the  $h$  and  $\rho$  variables are represented by solid and dashed lines, respectively, with a right arrow. Additionally there are diagrammatic definitions for the vertex and for the correlation functions for the  $h$  and  $\rho$  variables.

$$
S_h(k,\omega) = \frac{1}{\omega^2 + |\Sigma_h(k,\omega)|^2} \left[ 1 + \mu^2 \int \frac{dq}{2\pi} \int \frac{d\Omega}{2\pi} \left| k - q \right|^2 \right.
$$
  
 
$$
\times S_h(k-q,\omega-\Omega) S_\rho(q,\Omega) \right]
$$
(10a)

$$
\approx \frac{1}{\omega^2 + |\Sigma_h(k,\omega)|^2} \left[ 1 + \mu^2 \int \frac{dq}{2\pi} \int \frac{d\Omega}{2\pi} \right]
$$

$$
\times \frac{|k-q|^2}{|k-q|^{1+2\alpha_h}} \frac{1}{q^{1+2\alpha_\rho}} \left( \frac{2\Sigma_\rho(q,\Omega)}{\Omega^2 + |\Sigma_\rho(q,\Omega)|^2} \right)
$$

$$
\times \left( \frac{2\Sigma_h(k-q,\omega-\Omega)}{(\omega-\Omega)^2 + |\Sigma_h(k-q,\omega-\Omega)|^2} \right) \right]
$$
(10b)

$$
\approx \frac{1}{\omega^2 + |\Sigma_h(k,\omega)|^2} \left[ 1 + \mu^2 \int \frac{dq}{2\pi} \frac{|k-q|^{1-2\alpha_h}}{q^{1+2\alpha_\rho}} \right]
$$

$$
\times \left( \frac{\Sigma_\rho(q) + \Sigma_h(k-q)}{\omega^2 + (\Sigma_\rho(q) + \Sigma_h(k-q))^2} \right) \Bigg].
$$
 (10c)

The frequency-dependent self-energy  $\sum_h(k,\omega)$  in the above



FIG. 6. One-loop diagrams for (a)  $S_h(k,\omega)$ , the *h* – *h* correlation function, (b)  $S_\rho(k,\omega)$ , the  $\rho-\rho$  correlation function for the coupled equations of case  $B$  [Eq.  $(6)$ ].

is given by evaluating the integral over the internal frequency  $\Omega$  in Eq. (7b). This leads to

$$
\Sigma_h(k,\omega) \approx \mu^2 \int \frac{dq}{2\pi} \frac{k(k-q)}{q^{1+2\alpha_\rho}} \frac{A}{-i\omega + \Sigma_\rho(q) + \Sigma_h(k-q)}
$$
(11a)

$$
\approx \mu^2 \frac{A}{4\pi\alpha_\rho} \frac{k^2 k_0^{-2\alpha_\rho}}{-i\omega + \Gamma_0 k}
$$
 (11b)

$$
\approx \frac{\Gamma_0^2 k^2}{-i\omega + \Gamma_0 k},\tag{11c}
$$

where  $\Gamma_0 = \mu k_0^{-\alpha_p} \sqrt{A/4\pi\alpha_p}$ , and the second line in the above follows from taking a *q→*0 limit and introducing a cutoff wave vector  $k_0$  in the integral on the first line. Introducing this expression for  $\Sigma_h(k,\omega)$  in Eq. (10b) and recognizing that the divergence due to  $q^{-(1+2\alpha_\rho)}$  dominates the integral we find

$$
S_h(k,\omega) = \left(\omega^2 + \frac{\Gamma_0^4 k^4}{\omega^2 + \Gamma_0^2 k^2}\right)^{-1}
$$
  
 
$$
\times \left[1 + \frac{\mu^2 C_\rho}{4 \pi \alpha_\rho} k_0^{-2\alpha_\rho} \frac{k^2}{k^{1+2\alpha_h}} \frac{\Gamma_0 k}{\omega^2 + \Gamma_0^2 k^2}\right].
$$
 (12)

On integrating with respect to  $\omega$  we can write the structure factor  $S_h(k,t=0)$  as

$$
S_h(k,t=0) \equiv \int S_h(k,\omega) \frac{d\omega}{2\pi} = \frac{A_0}{k} + \frac{B_0}{k^{1+2\alpha_h}}.
$$
 (13)

Recognizing that the scaling form of  $S_h(k,t=0)$  $\sim k^{-1-\bar{2}\alpha_h}$ , we notice that  $\alpha_h$  cannot in general be determined from Eq.  $(13)$ . This is because the second term on the right-hand side of Eq.  $(13)$  dominates at small momenta  $k$ provided  $\alpha_h > 0$ , indicating that  $\alpha_h$  is indeterminate to this order of calculation.

We turn now to the critical exponents in  $\rho$ . The single loop self-energy  $\sum_{\rho}(k,\omega)$  is given as shown in Fig. 7(a) by

$$
\Sigma_{\rho}(k,\omega=0) = -\mu^2 \int \frac{dq}{2\pi} \int \frac{d\Omega}{2\pi} G_{\rho}(k-q,-\Omega) S_h(q,\Omega) q^2.
$$
\n(14)

Inserting the expressions for  $G_{\rho}(k-q,\omega-\Omega)$  and  $S_h(q,\Omega)$ we find

$$
\Sigma_{\rho}(k,\omega=0) = -\mu^2 \int \frac{dq}{2\pi} \int \frac{d\Omega}{2\pi} \left[ \frac{1}{i\Omega + |k-q|^{z_{\rho}}} \right]
$$

$$
\times \left[ \frac{2q^{z_h}}{\Omega^2 + q^{2z_h}} \right] \frac{q^2}{q^{1+2\alpha_h}}.
$$

This gives, on performing the integral over internal frequency  $\Omega$ ,

$$
\Sigma_{\rho}(k,\omega=0) = -\mu^2 \int \frac{dq}{2\pi} \frac{q^2}{q^{1+2\alpha_h}} \frac{1}{|k-q|^{z_{\rho}}+q^{z_h}}.
$$

In order to discuss this further in the context of  $z<sub>0</sub>$ , we need to make a statement about  $\alpha_h$  and  $z_h$ . We have already obtained  $z_h=1$  in the foregoing and will now quote our numerical result for  $\alpha_h$ , viz.,  $\alpha_h$ =0.5. For small *k* the selfenergy can then be written as

$$
\Sigma_{\rho}(k,\omega) \approx -\mu^2 \left[ \int \frac{dq}{2\pi} \frac{1}{(q+q^{z_{\rho}})}
$$

$$
+ z_{\rho} k \int \frac{dq}{2\pi} \frac{1}{(q+q^{z_{\rho}})(q+q^{2z_{\rho}})} \right].
$$

We see from the above that  $\sum_{\rho}(k,0)$ , the relaxation rate for  $\rho$ fluctuations, is negative and finite as  $k\rightarrow 0$ , and we need to add a positive constant,  $\Sigma_0$ , to the self-energy  $[\Sigma_0 > \Sigma_0(k)]$  $\rightarrow$ 0)<sup>|</sup>] for regulatory purposes. This divergence in the relaxation rate, needing regulation, is reflected in the divergence we have encountered in our numerical investigations below; we have there followed an analogous procedure by introducing a numerical regulator that replaces divergent values of the transfer term by suitably defined cutoffs  $[5]$ . The resulting constancy of  $\Sigma_{\rho}$  implies  $z_{\rho} \approx 0$  for the regulated equations and will be used in the following.

The correlation function  $S_\rho(k,\omega)$  is given by [Fig. 6(b)]

$$
S_{\rho}(k,\omega) = \frac{1}{(\omega^2 + k^{2z_{\rho}})} \int \frac{dq}{2\pi}
$$
  
 
$$
\times \int \frac{d\Omega}{2\pi} (k-q)^2 S_h(k-q,\omega-\Omega) S_{\rho}(q,\Omega).
$$

The above integral will now be evaluated in the limit *q*  $\rightarrow$ 0 and since  $\Omega \sim q^{z_h}$  for  $S_h$  we can replace

$$
S_h(k-q,\omega-\Omega) \approx S_h(k,\omega).
$$

Then using the scaling relation Eq.  $(3)$  we have

$$
S_{\rho}(k,\omega) \simeq \frac{1}{(\omega^2 + k^{2z_{\rho}})} \int \frac{dq}{2\pi} \frac{C_{\rho}}{q^{1+2\alpha_{\rho}}} k^2 S_h(k,\omega) \quad (15a)
$$

$$
= \frac{k^2 C_{\rho}}{(\omega^2 + k^{2z_{\rho}})} S_h(k,\omega) \int \frac{dq}{2\pi} \frac{1}{q^{1+2\alpha_{\rho}}}
$$

$$
C^{-1} k^{-2\alpha_{\rho}} \qquad k^{1-2\alpha_{h}+z_{h}} \qquad (15b)
$$

$$
=\frac{C_{\rho}k_{0}^{-2\alpha_{\rho}}}{4\pi\alpha_{\rho}}\frac{k^{1-2\alpha_{h}+z_{h}}}{(\omega^{2}+k^{2z_{\rho}})(\omega^{2}+k^{2z_{h}})},
$$
\n(15c)

where the last step follows from introducing a lower cutoff  $k_0$  in the momentum integration over  $q$ .

Using Eq. (3) we have after integrating Eq. (15c) over  $\omega$ 

$$
S_{\rho}(k,t=0) \sim k^{-(1+2\alpha_{\rho})} \sim \frac{k^{1-2\alpha_h}}{k^{z_{\rho}}(k^{z_h} + k^{z_{\rho}})}.
$$
 (16)

Finally using  $z_0 \approx 0$  we have

$$
\alpha_{\rho} = \begin{cases} \alpha_h + \frac{z_h}{2} - 1 & \text{for large } k \\ 1 & \text{for small } k \end{cases}
$$
 (17a)

 $\left( \alpha_h - 1 \right)$  for small *k*.  $(17b)$ 

Given our numerical result of  $\alpha_h=0.5$ , the above predicts a negative  $\alpha_{\rho}$ , at small *k*. This is consistent with, and validates our assumption of, a cutoff  $k_0$  that arises naturally as the wave vector separating the region of  $\alpha_{\rho} < 0$  (no infrared divergence) and  $\alpha_{\rho}$  > 0 (infrared divergence prevalent) in Eqs.  $(7b)$  and  $(10c)$ .

More importantly, this nontrivial result for  $\alpha_{\rho}$  indicates that should we see numerical evidence of a negative  $\alpha_{\rho}$  for small wave vectors, we will have verified the existence of an asymptotic hypersmoothing in our model equations, which has an important bearing on sandpile surfaces in the continuous avalanching regime. This is discussed further in our concluding section.

#### **B. Numerical analysis**

We focus now on our numerical results for case *B*. The coupled equations in this section and the following one were numerically integrated by using the method of finite differences  $[22]$ . Our grids in time and space were kept as fine grained as computational constraints allowed so that our grid size in space  $\Delta x$  was chosen to be in the range  $(0.1,0.5)$ whereas that in time was in the range  $\Delta t$   $(0.001, 0.005)$ .



FIG. 7. Log-log plot of the single Fourier transform  $S_h(k,t=0)$  vs *k* obtained from Eqs. (6) (case *B*). The best fit has a slope of  $-1$  $-2\alpha_h = -2.03 + \pm 0.014$ . Other parameters are  $\mu = D_h = D_\rho = \frac{\Delta_h^2}{\Delta_h^2} = \frac{\Delta_f^2}{\Delta_f^2} = 1.0$ .

Thus the instabilities associated with the discretization of nonlinear continuum equations were avoided and convergence was checked by keeping  $\Delta t$  small enough such that the quantities under investigation were independent of further discretization. Our results were also checked for finite size effects. In the calculations of this section we chose  $D<sub>h</sub>$  $= D<sub>0</sub>=1.0$  and  $\mu = 1$  and our results were averaged over several independent configurations. We have calculated the exponents  $\alpha$  and  $\beta$  and the corresponding error bars using the linear least square fit so that  $-(1+2\beta)$  and  $-(1$  $+2\alpha$ ) are given by slopes of the fitted straight lines.

On discretizing Eqs.  $(6)$  we found once again the divergences that were previously observed in  $[5]$ . These divergences are in our view a direct representation of the infrared divergence mentioned above, and we follow here a parallel course in regulating these via an explicit regulator. In earlier work  $[5]$ , a regulator was introduced that replaced the function  $\mu \rho \nabla h$  by the following:

$$
T = \begin{cases} +1 & \text{for } \mu \rho(\nabla h) > 1 \\ \mu \rho(\nabla h) & \text{for } -1 \leq \mu \rho(\nabla h) \leq 1 \\ -1 & \text{for } \mu \rho(\nabla h) < -1 \end{cases}
$$

In addition in this paper, we have introduced noise reduction to the regulated equations, which has led to a more accurate evaluation of all our critical exponents.

The Fourier transform  $S_h(k,t=0)$  (Fig. 7) is consistent with a spatial roughening exponent  $\alpha_h \sim 0.501 \pm 0.007$  via our observation of

$$
S_h(k, t=0) \sim k^{-2.03 \pm 0.014}
$$



FIG. 8. Log-log plot of the single Fourier transform  $S_h(x=0,\omega)$  vs  $\omega$  for case *B* obtained from Eqs. (6). The best fit shown in the figure has a slope of  $-1-2\alpha_h=1.93\pm0.017$ . Again  $\mu = D_h = D_\rho = \Delta_h^2 = \Delta_\rho^2 = 1.0$ .



FIG. 9. The double Fourier transform  $S_h(k_i, \omega)$  vs  $\omega$  (case *B*) calculated at two different wave vectors  $k_i = 0.1$  ( $\Diamond$ ), 0.2 (+). The curves [solid (1) and dashed (2) lines] shown in the figure are plots of Eq. (18) with  $\Gamma_0=0.4$  and 0.5 (for  $k_1$  and  $k_2$ , respectively), to serve as a guide to the eye. Other parameters are  $\mu=2$ ,  $\Delta_h^2 = \Delta_\rho^2 = 0.1$ ,  $D_h = D_\rho = 1.0$ .

and the Fourier transform  $S_h(x=0,\omega)$  (Fig. 8) is consistent with a temporal roughening exponent  $\beta_h$  ~ 0.465 ± 0.008 via our observation of

$$
S_h(x=0,\omega) \sim \omega^{-1.93 \pm 0.017}
$$
.

Hence  $z_h \sim 1.07$ , and thus the exponent  $x_\mu \approx 0$  [Eq. (9)], indicating that the  $\mu$  vertex does not renormalize.

Using  $\alpha_h \sim 0.5$  in Eq. (12) we can write the structure factor  $S_h(k,\omega)$  as

$$
S_h(k,\omega) = \frac{1}{1 + \Omega^2 (1 + \Omega^2)} \left[ \frac{1 + \Omega^2}{\Gamma_0^2 k^2} + \frac{1}{\Gamma_0 k^3} \right],
$$
 (18)

where  $\Omega = \omega / \Gamma_0 k$ . We find from the above that the expected form of  $S_h(k, \omega=0)$  in the limit of small wave vectors is

$$
S_h(k, \omega = 0) \sim k^{-3}.
$$
 (19)

Realizing that our computed  $\alpha_h$ <1, we obtain from Eq. (12) the prediction

$$
S_h(k=0,\omega) \sim \omega^{-2}.
$$
 (20)

The full structure factor  $S_h(k,\omega)$  has been calculated at two different *k* points and Fig. 9 displays our results fitted to Eq. (18). The solid and the dashed line in Fig. 9 are the plots of Eq. (18) for  $k=0.1$  and  $k=0.2$  with  $\Gamma_0=0.4$  and 0.5, respectively. The spatial structure factor  $S_h(k, \omega=0)$  shows a power-law behavior (Fig. 10) given by

$$
S_h(k, \omega = 0) \sim k^{-3.40 \pm .029}
$$



FIG. 10. Log-log plot of the double Fourier transform  $S_h(k, \omega = 0)$  vs *k* (case *B*) obtained from Eqs. (6). The best fit has a slope of  $(1+2\alpha_h + z_h) = -3.40 \pm 0.029$ . Again,  $\mu = 1.0$ ,  $D_h = D_\rho = 1.0$ ,  $\Delta_h^2 = \Delta_\rho^2 = 0.5$ .



FIG. 11. Log-log plot of the double Fourier transform  $S_h(k=0,\omega)$  vs  $\omega$  obtained from Eqs. (6) (case *B*). The best fit displayed in the figure has a slope of  $-(1+2\beta_h+1/z_h) = -1.91 \pm 0.017$ . Other parameters are  $\mu = 1.0$ ,  $D_h = D_\rho = 1.0$ ,  $\Delta_h^2 = \Delta_\rho^2 = 0.5$ .

in qualitative accord with Eq.  $(19)$ , and the temporal structure factor  $S_h(k=0,\omega)$  shows a power-law behavior (Fig. 11) given by

$$
S_h(k=0,\omega) \sim \omega^{-1.91 \pm .017}
$$

in accord with Eq.  $(20)$ .

Given our values of  $\alpha_h \approx 0.5$  and  $z_h \approx 1$ , Eqs. (17a) and (17b) predict a crossover in  $\alpha_{\rho}$  from 0 at large *k* to -0.5 as  $k \rightarrow 0$ . The single Fourier transform  $S_{\rho}(k,t=0)$  (Fig. 12) shows a crossover behavior from

$$
S_{\rho}(k,t=0) \sim k^{-2.12 \pm 0.017}
$$

for large wave vectors to

$$
S_{\rho}(k,t=0) \sim \text{const}
$$

as *k→*0. In Fig. 12 we find a crossover from 0.56 at large *k* to  $-0.5$  as  $k\rightarrow 0$ , which shows the same trend as the prediction above. Note, however, that the simulations also manifest, in addition to the theoretical predictions, the normal diffusive behavior represented by  $\alpha_p = 0.56$  at large wave vectors. The single Fourier transform in time  $S_p(x=0,\omega)$ (Fig. 13) shows a power-law behavior:

$$
S_{\rho}(x=0,\omega) \sim \omega^{-1.81 \pm 0.017}.
$$

While the range of wave vectors in Fig. 12 over which crossover in  $S_p(k,t=0)$  is observed was restricted by our computational constraints, the form of the crossover appears conclusive. Checks (with fewer averages) over larger system sizes revealed the same trend; additionally our theoretical calculations support the observed crossover via Eqs.  $(17)$ .



FIG. 12. Log-log plot of the single Fourier transform  $S_\rho(k,t=0)$  vs *k* (case *B*) showing a crossover from a slope of  $-1-2\alpha_\rho=0$  at small *k* to  $-2.12 \pm 0.017$  at large *k*. Other parameters are  $\mu = 1.0$ ,  $D_h = D_\rho = 1.0$ ,  $\Delta_h^2 = \Delta_\rho^2 = 0.5$ .



FIG. 13. Log-log plot of the single Fourier transform  $S_\rho(x=0,\omega)$  vs  $\omega$  obtained from Eqs. (6) (case *B*). The best fit has a slope of  $-1-2\beta_{\rho} = -1.81 \pm 0.017$ . Again,  $\mu = 1.0$ ,  $D_h = D_{\rho} = 1.0$ ,  $\Delta_h^2 = \Delta_{\rho}^2 = 0.5$ .

#### **C. Homing in on the physics: A discussion of smoothing**

We focus in this section on the physics of the equations and our results. In the regime of continuous avalanching in sandpiles, the major dynamical mechanism is that of mobile grains  $\rho$  present in avalanches flowing into voids in the  $h$ landscape as well as the converse process of unstable clusters (a surfeit of  $\nabla h$  above some critical value) becoming destabilized and adding to the avalanches. Our results for the critical exponents in *h* indicate no further spatial smoothing beyond the diffusive; however, those in the species  $\rho$  indicate a crossover from purely diffusive to an asymptotic hypersmooth behavior. Our claim for continuous avalanching is as follows: the flowing grains play the major dynamical role as all exchange between  $h$  and  $\rho$  takes place only in the presence of  $\rho$ . These flowing grains therefore distribute themselves over the surface filling in voids in proportion both to their local density as well as to the depth of the local voids; it is this distribution process that leads in the end to a strongly smoothed profile in  $\rho$ . Additionally, since in the regime of continuous avalanches, the effective interface is defined by the profile of the *flowing* grains, it is this profile that will be measured experimentally for, say, a rotating cylinder with high velocity of rotation.

### **IV. ANOMALOUS SMOOTHING: THE CASE OF TILT** AND BOUNDARY-LAYER EXCHANGE (CASE *C*)

The last case we discuss in this paper involves a more complex coupling between the stuck grains *h* and the flowing grains  $\rho$  as follows:

$$
\frac{\partial h(x,t)}{\partial t} = D_h \nabla^2 h(x,t) - T + \eta(x,t),\tag{21a}
$$

$$
\frac{\partial \rho(x,t)}{\partial t} = D_{\rho} \nabla^2 \rho(x,t) + T,\tag{21b}
$$

$$
T(h,\rho) = -\nu(\nabla h)_{-} - \lambda \rho(\nabla h)_{+}
$$
 (21c)

with  $\eta(x,t)$  representing white noise as usual.

Here,

$$
z_{+} = \begin{cases} z & \text{for } z > 0 \\ 0 & \text{otherwise,} \end{cases}
$$
 (22a)

$$
z_{-} = \begin{cases} z & \text{for } z < 0 \\ 0 & \text{otherwise.} \end{cases}
$$
 (22b)

This equation was also presented in earlier work  $[5]$  in the context of the surface dynamics of an evolving sandpile. The two terms in the transfer term *T* represent two different physical effects which we will discuss in turn. The first term represents the effect of tilt, in that it models the transfer of particles from the boundary layer at the ''stuck'' interface to the flowing species whenever the local slope is steeper than some threshold (in this case zero, so that negative slopes are penalized). The second term is restorative in its effect, in that in the presence of "dips" in the interface (regions where the slope is shallower, i.e., more positive than the zero threshold used in these equations), the flowing grains have a chance to resettle on the surface and replenish the boundary layer  $[2]$ . We notice that because one of the terms in  $T$  is independent of  $\rho$  we are no longer restricted to a coupling that exists only in the presence of flowing grains: i.e., this model is applicable to intermittent avalanches when  $\rho$  may or may not always exist on the surface. In the following we examine the effect of this interaction on the profiles of  $h$  and  $\rho$ , respectively.

The complexity of the transfer term with its discontinuous functions precludes any attempts to solve this model along the lines of the earlier ones. We make some remarks here, however, on the likely critical behavior of this model.

We observe that the transfer term

$$
T = -\lambda \rho (\nabla h)_{+} - \nu (\nabla h)_{-}
$$

can be thought of as a formal infinite series by invoking a suitable representation for the Heaviside step functions in



 $(b)$ 

FIG. 14. One-loop corrections to  $(a)$  the KPZ vertex, and  $(b)$  the  $\lambda$  vertex for the coupled equations of case *C* [Eqs. (21)].

Eq.  $(23)$ . We are then led to consider the following more general structure for the transfer term *T*,

$$
T = -\lambda \rho (\nabla h) - \nu (\nabla h) - \sum_{n=1}^{\infty} \nu_n (\nabla h)^{n+1}
$$

$$
- \rho \sum_{n=1}^{\infty} \lambda_n (\nabla h)^{n+1}.
$$
 (23)

Note, however, that this is not a very well-defined expansion because the coefficients in the infinite series could well be very large, if not infinite. However, given this disclaimer, we can still make the following comments in the spirit of selfconsistency, i.e., subject to numerical verification.

If  $\lambda \rho(\nabla h)$  were the only nonlinearity, as in case *B*, we would have  $z_h=1$ . Using  $h \sim x^{\alpha_h}$  and  $\rho \sim x^{\alpha_p}$ , we see  $\lambda \rho(\nabla h)$  is a more relevant nonlinearity than  $\nu_1(\nabla h)^2$ , the leading nonlinear term in the expansion of  $(\nabla h)$ <sub>-</sub>, and is likely to be the controlling nonlinearity for the extreme long wavelength behavior. Figure 14 shows that the  $\lambda$  vertex never renormalizes in the presence of the KPZ term  $\nu_1(\nabla h)^2$ , so that  $z_h$  is always fixed at unity. However, the KPZ vertex corresponding to  $\nu_1(\nabla h)^2$  has distinct behavior in different wave vector ranges. In the range where the vertex renormalizes, we cannot say much about the behavior of  $\alpha_h$ ; however, in the range where it does *not* renormalize, we might imagine that normal KPZ hyperscaling  $\alpha_h + z_h = 2$ would be restored. This, with  $z_h=1$ , would give  $\alpha_h=1$ .

If  $z_h=1$ , we can write the scaling relation  $S_h(k,\omega=0)$  for the double Fourier transform at zero frequency as

$$
S_h(k,\omega=0)\sim k^{-2-2\alpha_h},
$$

which, in the regime where the KPZ hyperscaling holds, should look like  $S_h(k, \omega=0) \sim k^{-4}$ .

We now try to obtain additional insights into the behavior of these equations using the Hartree-Fock approximation. The spirit of the Hartree-Fock approximation is to replace nonlinear terms by linear ones with coefficients that are generally determined self-consistently. To undertake that here, we note that the step functions  $[Eq. (23)]$  give rise to nonlinearities and hence the simplest thing to do is to replace them by an expectation value (the argument of the step function is a random variable and hence this is an acceptable approximation). We represent this expectation value by a number *c* with  $0 < c < 1$ . The equations of motion thus read

$$
\frac{\partial h}{\partial t} = D_h \nabla^2 h - \lambda' \rho \nabla h - \nu' \nabla h + \eta_h(x, t), \qquad (24a)
$$

$$
\frac{\partial \rho}{\partial t} = D_{\rho} \nabla^2 \rho + \lambda' \rho \nabla h + \nu' \nabla h, \qquad (24b)
$$

with  $\lambda' = c\lambda$  and  $\nu' = (1 - c)\nu$  and are identical to the ones studied by Bouchaud *et al.* [7]. We expect at least in some regime of Eqs.  $(21)$  to reproduce the mean-field results appropriate to Eqs.  $(24a)$  and  $(24b)$ .

### *1. Results for the single Fourier transforms*

The single Fourier transforms  $S_h(k,t=0)$  (Fig. 15) and  $S_h(x=0,\omega)$  (Fig. 16) show power-law behavior corresponding to

$$
S_h(k, t=0) \sim k^{-2.56 \pm 0.060},
$$
  

$$
S_h(x=0, \omega) \sim \omega^{-1.68 \pm 0.011},
$$

which implies that the roughness and the growth exponents are given respectively by  $\alpha_h = 0.78 \pm 0.030$  and  $\beta_h = 0.34$  $\pm$  0.005. This suggests  $z_h = \alpha_h / \beta_h \approx 2$ , contradicting the prediction of  $z_h$ =1 by perturbative methods and suggesting that the mean-field approach outlined in the above might be more appropriate. We discuss this further in what follows.

However, the small *k* limit of  $S_h(k,t=0)$  indicates a downward curvature and thus a deviation from the linear behavior at higher  $k$  (Fig. 15). This curvature, which had also been observed in previous work  $[5]$ , indicates a smaller roughness exponent  $\alpha_h$  there, i.e., an asymptotic *smoothing*.

### *2. Results for the double Fourier transforms*

The double Fourier transforms  $S_h(k, \omega=0)$  (Fig. 17) and  $S_h(k=0,\omega)$  (Fig. 18) show power-law behavior corresponding to

$$
S_h(k=0,\omega) \sim \omega^{-1.80\pm0.007},
$$
  

$$
S_h(k,\omega=0) \sim \begin{cases} k^{-4.54\pm0.081} & \text{for large wave vectors} \\ \text{const} & \text{for small wave vectors.} \end{cases}
$$

The double Fourier transform  $S_h(k=0,\omega)$  shows the usual  $\omega^{-2}$  behavior that we have seen before in Eqs. (5) and  $(20)$ , which we have already discussed earlier.

The structure factor  $S_h(k,\omega=0)$  signals a dramatic behavior of the roughening exponent  $\alpha_h$ , which crosses over



FIG. 15. Log-log plot of the single Fourier transform  $S_h k$ ,  $t = 0$ ) vs  $k$  for case  $C$  obtained from Eqs. (21). The slope of the fitted line is given by  $-1-2\alpha_h = -2.56\pm0.060$ . The parameters used in the simulation are  $\nu = 10$ ,  $\lambda = 1.0$ ,  $D_h = D_\rho = 1.0$ ,  $\Delta_h^2 = 1.0$ .

from  $(i)$  a value of 1.3 indicating anomalously large roughening at intermediate wave vectors, to (ii) a value of about  $-1$  for small wave vectors indicating asymptotic hypersmoothing.

The anomalous roughening  $\alpha_h=1$  seen here is consistent with that observed via the single Fourier transform  $(Fig. 15)$ and suggests, via the perturbative arguments given previously, that  $z_h=1$ . However, if we assume  $z_h=2$  according to the results of the single Fourier transforms given above, this would lead to an  $\alpha_h$  of about 0.8, in agreement with the values obtained both via single Fourier transforms in the present paper, and in [5]. In either case, our values of  $\alpha_h$  $(either 1.3 or 0.8)$  suggest anomalous roughening of the interface at moderately large wave vectors.

The anomalous smoothing obtained here ( $\alpha_h \sim -1$  if  $z_h$ )  $\sim$  1, and  $\alpha_h$  $\sim$  - 1.5 in the event that  $z_h$  is taken to be 2) is also consistent with the downward curvature in the single Fourier transform  $S_h(k,t=0)$ , as both imply a negative  $\alpha_h$ ; we mention also that the wave vector regime where this smoothing is manifested is almost identical in both Figs. 15 and 17.

Since we expect that the anomalous smoothing results from a failure of the expansion of the step functions along the lines of Eq.  $(23)$ , this underlines our expectation that the mean-field solution of Eqs.  $(24a)$  and  $(24b)$  would capture at least some of the flavor of this regime. We have therefore solved the mean-field equations [Eqs.  $(24a)$  and  $(24b)$ ] numerically, and from Fig. 19 and Fig. 20 we find that there is a crossover in  $S_h(k,t=0)$  (Fig. 19) from a diffusive behavior  $(z_h=2)$  at high wave vectors to a smoothing behavior at low wave vectors.

This behavior is reflected in our results for case *C*. At low



FIG. 16. Log-log plot of the single Fourier transform  $h(x=0,\omega)$  vs  $\omega$  obtained from Eqs. (21) (case *C*). The best fit has a slope of  $-1-2\beta_h = -1.68 \pm 0.011$  with parameters  $\nu=10$ ,  $\lambda=1.0$ ,  $D_h = D_\rho = 1.0$ ,  $\Delta_h^2 = 1.0$ .



FIG. 17. Log-log plot of the double Fourier transform  $S_h(k, \omega = 0)$  vs *k* obtained from Eqs. (21) (case *C*). The best fit for high wave vector has a slope of  $-(1+2\alpha_h+\zeta_h)=-4.54\pm0.081$ . As  $k\rightarrow 0$  we observe a crossover to slope of zero. Other parameters are  $D_h=D_\rho$ = 1.0,  $\Delta_h^2$  = 1.0,  $\nu$  = 10, and  $\lambda$  = 1.0.

frequencies the region of anomalous smoothing can be understood by comparison with the corresponding region in the mean-field equations Eqs.  $(24a)$  and  $(24b)$ , which also manifest this. At large *k*,  $S_h(k,t=0)$  and  $S_h(k,\omega=0)$  indicate anomalous roughening with  $\alpha_h \approx z_h \approx 1$ , which is consistent with the infrared divergence discussed in the previous section. However, as in case A,  $S_h(x=0,\omega)$  is dominated by the diffusive  $z_h=2$  arising from the presence of  $\delta(\omega-\nu'k)$  in the mean-field solution of case *C*. This behavior is corroborated by an evaluation of the full structure factor  $S(k_i, \omega)$ (Fig. 21) which shows a distinct peak at an  $\omega_i$  given by  $\omega_i$  $= v' k_i$ ; this is reminiscent of the Lorentzian obtained in case *A* (Fig. 1). In fact, to leading order,  $S_h(k,\omega)$  can be fitted to a Lorentzian; however, as we reduce the relative strength of  $\nu(\nabla h)$  with respect to  $\lambda \rho(\nabla h)$  the Lorentzian peaks disappear, and we begin to see a ''shoulder'' reminiscent, as it should be, of the behavior observed in case  $B$  (Fig. 9). This suggests that the present model is an integrated version of the earlier two, reducing to their behavior in different wave vector regimes; we speculate therefore that there are *two* dynamical exponents  $(z_h=1 \text{ and } z_h=2)$  in the problem.

# **V. DISCUSSION AND CONCLUSIONS**

We have presented in the above a discussion of three models of sandpiles, all of which manifest asymptotic smoothing: cases *A* and *C* manifest this in the species *h* of stuck grains, while case  $B$  manifests this in the species  $\rho$  of flowing grains. We reiterate that the fundamental physical



FIG. 18. Log-log plot of the double Fourier transform  $S_h(k=0,\omega)$  vs  $\omega$  obtained from Eqs. (21) (case *C*). The best fitted line shown in the figure has a slope of  $-(1+2\beta_h+1/z_h) = -1.80 \pm 0.007$ . Other parameters are  $D_h = D_\rho = 1.0$ ,  $\Delta_h^2 = 1.0$ ,  $\nu = 10$ , and  $\lambda = 1.0$ .



FIG. 19. Log-log plot of the single Fourier transform  $S_h(k, t = 0)$  vs *k* obtained from the mean-field Eqs. (24a) and (24b). The high-*k* region is fitted with a line of slope  $-1-2\alpha_h = -2.05 \pm 0.017$ . The low-*k* region is fitted with a line of slope  $-1-2\alpha_h = -0.93 \pm 0.024$ . Note the crossover from  $\alpha_h = 0.5$  at large *k* to zero at small *k*. Other parameters are  $\nu' = 10$ ,  $\lambda' = 2.0$ ,  $D_h = D_\rho = 1.0$ ,  $\Delta_h^2 = 0.1$ .

reason for this is the following: cases *A* and *C* both contain couplings that are independent of the density  $\rho$  of flowing grains, and are thus applicable, for instance, to the dynamical regime of intermittent avalanching in sandpiles, when grains occasionally but not always flow across the ''bare'' surface. In case  $B$ , by contrast, the equations are coupled only when there is continuous avalanching, i.e., in the presence of a finite density  $\rho$  of flowing grains.

The analysis of case *A* is straightforward, and was undertaken really only to explain features of the more complex case *C*; that of case *B* shows satisfactory agreement between perturbative analysis and simulations. Anomalies persist, however, when such a comparison is made in case *C*, because the discontinuous nature of the transfer term makes it analytically intractable. These are removed when the analysis includes a mean-field solution that is able to reproduce the asymptotic smoothing observed.

We suggest therefore an experiment where the critical roughening exponents of a sandpile surface are measured in

- $(1)$  a rapidly rotated cylinder, in which the time between avalanches is much less than the avalanche duration. Our results predict that for small system sizes we will see only diffusive smoothing, but that for large enough systems, we will see extremely smooth surfaces.
- $(2)$  a slowly rotated cylinder where the time between avalanches is much more than the avalanche duration. In this regime, the results of case *C* make a fascinating prediction: anomalously large spatial roughening for moderate system sizes crossing over to an anomalously large spatial smoothing for large systems.



FIG. 20. Log-log plot of the single Fourier transform  $S_h(x=0,\omega)$  vs  $\omega$  for the mean-field Eqs. (24a) and (24b). The best fit has a slope of  $-1-2\beta_h = -1.94 \pm 0.001$  with parameters  $\nu' = 10$ ,  $\lambda' = 2.0$ ,  $D_h = D_\rho = 1.0$ ,  $\Delta_h^2 = 0.1$ .



FIG. 21. The double Fourier transform  $S_h(k_i, \omega)$  vs  $\omega$  obtained from Eqs. (21) (case C) evaluated at three different wave vectors  $k_1$ = 0.2 ( $\Diamond$ ),  $k_2$ =0.4 (+), and  $k_3$ =0.8 ( $\Box$ ) with parameters  $D_h = D_\rho = 1.0$ ,  $\Delta_h^2 = 1.0$ ,  $\nu = 5$ , and  $\lambda = 1.0$ . The peaks correspond to frequencies  $\omega_1=1.0$ ,  $\omega_2=2.0$ ,  $\omega=4.0$ .

Finally we make some speculations in this context concerning natural phenomena. The qualitative behavior of blown sand dunes  $[23]$  is in accord with the results of case *B*, because sand moves swiftly and virtually continuously across their surface in the presence of wind. By contrast, on the surface of a glacier, we might expect the sluggish motion of boulders to result in intermittent flow across the surface, making the results of case *C* more applicable to this situation. It would be interesting to see if the predictions of anomalous roughening at moderate, and anomalous smoothing at large, length scales is applicable here.

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### **APPENDIX**

In this appendix we discuss some of the technical points related with the double Fourier transform. We have found that the crossover that we have seen in the Eq.  $(5)$  would not have been observed had we been using the single Fourier transforms  $S_h(k,t=0)$  and  $S_h(x=0,\omega)$  for numerical purposes. We illustrate this by writing explicitly the expressions for the relevant quantities:



FIG. 22. Log-log plot of the single Fourier transform  $S_h(k,t=0)$  vs *k* obtained from Eq. (4a) (case *A*) with parameters  $c = D_h = \Delta^2$ = 1.0. The best fitted line shown in the figure is given by a slope of  $-1-2\alpha_h = -1.90 \pm 0.016$ . The characteristic wave vector  $k_0$  is given by  $k_0 = c/D_h = 1.0$ .



FIG. 23. (a) Log-log plot of the single Fourier transform  $S_h(x=0,\omega)$  vs  $\omega$  obtained from Eq. (4a) showing a slow crossover. Lines 1 and 2 in the figure are the best fits in the low and high  $\omega$  regions with slopes  $-1-2\beta_h=-1.87\pm0.003$  and  $-1-2\beta_h=-1.525\pm0.006$ , respectively. (b) Log-log plot of the single Fourier transform  $S_h(x=0,\omega)$  vs  $\omega$  for two different values of *c*; *c* = 10 and *c* = 5 for data sets 1 and 2, respectively. Note the increase in oscillation for increasing values of *c*. The other parameters are  $D_h = \Delta^2 = 1.0$ .

$$
S_h(k, t=0) \sim k^{-2} \tag{A1a}
$$

$$
\left(\begin{array}{cc} & \alpha^{-2} & \text{for } \omega \text{ small} \end{array}\right) \qquad \text{(A1b)}
$$

$$
S_h(x=0,\omega) \sim \begin{cases} \omega & \text{for } \omega \text{ shan} \\ \omega^{-1.5} & \text{for } \omega \text{ large.} \end{cases}
$$
(A1c)

The examination of  $S_h(k,t=0)$  (Fig. 22) on its own yields no indication of the crossover to the smoothing fixed point; although there is a crossover in the  $S_h(x=0,\omega)$  graph [Fig. 23(a)] from  $\omega^{-1.5}$  to  $\omega^{-2}$ , the analysis below shows that *both* regimes reflect diffusive behavior, so that the smoothing fixed point ( $\alpha_h$ =0, $\beta_h$ =0, $z_h$ =1) is entirely suppressed.

The single Fourier transform  $S_h(x, \omega)$  is defined by

$$
S_h(x=0,\omega) = \int_{-\infty}^{\infty} \frac{dk}{2\pi} S_h(k,\omega)
$$

$$
= \int_{-\infty}^{\infty} \frac{dk}{2\pi} \frac{1}{D_h k^{z_h}} \left[ \frac{D_h k^{z_h}}{(\omega - ck)^2 + D_h^2 k^{2z_h}} \right].
$$

In the limit  $\omega \rightarrow c k$  the term in the square brackets behaves like a  $\delta$  function and thus

$$
S_h(x=0,\omega) = \int_{-\infty}^{\infty} \frac{dk}{2\pi} \frac{1}{D_h k^{z_h}} \delta(\omega - ck) \approx \frac{1}{\omega^{z_h}}.
$$
 (A2)

This is the origin of ballistic behavior in the flow term and is responsible for two anomalies.

(1) Firstly, we notice from the above that the  $\delta$  function causes  $S_h(x=0,\omega)$  to behave like  $\omega^{-z_h}$ . Comparing with Eq. (A1b) this leads to  $z_h$ =2. However a simple-minded application of Eqs. (3) would have led to the *wrong* conclusion of  $\beta_h$ =0.5. Even if the correct scaling relation Eq. (A2) were employed, the ballistic nature of the flow term picks out, misleadingly, the *high* frequency (diffusive) dynamical exponent in the *low* frequency regime of  $S_h(x=0,\omega)$  [Eq. (A1b)]. The low wave vector, low-frequency smoothing behavior is thus entirely suppressed.

 $(2)$  Secondly, spurious oscillations are observed [Fig. 23(b)] in the graph for  $S_h(x=0,\omega)$  as a function of grid size. A consideration of the form of the structure factor  $S_h(x)$  $=0,\omega$ ) makes it clear the crossover from small to large  $\omega$ should not involve any imaginary quantities, and therefore strictly speaking we should not see any oscillatory behavior in the structure factor in this limit. However, the full form of the structure factor  $S_h(x, \omega)$  for finite *x does* contain imaginary portions, which are responsible for the oscillations. The characteristic length and time scales in our problem are given by

$$
t_0 = D_h/c^2
$$
,  $x_0 = D_h/c$ .

Whenever grid sizes in time or space are comparable to these characteristic lengths, the profile fluctuates across these intervals, which is then aggravated by the shock fronts associated with the flow term. This results in oscillatory behavior arising from the *nonzero* intervals in *x* associated with the sampling of the profile to generate the Fourier transform,  $S_h(x=0,\omega)$ , which introduce a flavor of  $S_h(x,\omega)$  for *finite x*. These become increasingly violent as *c* increases because of the increased fluctuations associated with the ballistic flow term over the grids. In order to avoid these oscillations, one should choose grid sizes  $\Delta x$  and  $\Delta t$  in such a way that they are always less than the characteristic scales in the problem, i.e.,

$$
\Delta x{\ll}x_0 \text{ and } \Delta t{\ll}t_0.
$$

In view of the above, it is necessary to use the double Fourier transform to obtain an unambiguous picture of the structure factor and to pick out the asymptotic smoothing although this strategy might on first appearance seem to be a computational overkill. The overwhelming advantage is that, by scanning the structure factor as a function of frequency  $\omega$  for a fixed *k*, one immediately sets two frequency scales *ck* and  $D_h k^2$ , thus making it possible to pick up the relevance of these scales in  $S_h(k,\omega)$ . We also mention that our discussion is equally applicable to the Kardar-Parisi-Zhang equation  $[17]$  with the addition of a flow term. Here too, the use of the double Fourier transform reveals the presence of the ''smoothing'' fixed point due to the flow term.

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